

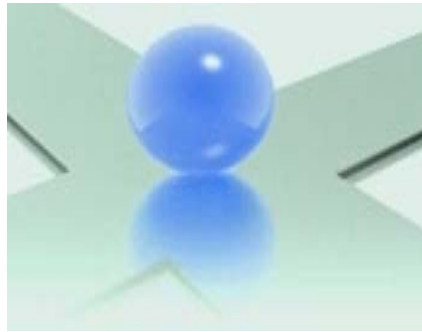
Lecture 4

Vibration Suppression with Uncertain Load

Yakov Ben-Haim

Technion

Israel Institute of Technology



Contents

1	Highlights (tufts2025lec04-001.tex)	3
2	Design of a Vibrating Cantilever (vib-con02.tex)	10
2.1	Design Problem	10
2.2	Robustness Function	16
2.3	Numerical Example	39
2.4	Opportuneness Function	48
2.5	Summary of Vibrating Cantilever Example	56
3	Summary (tufts2025lec04-001.tex)	65

1 *Highlights*

- **Models:**
 - **Conflicting.**
 - **Simplistic.**
 - **Incomplete.**
-

- **Models:**
 - Conflicting.
 - Simplistic.
 - Incomplete.
- **Data:**
 - Random.
 - Biased, unknown correlations.
 - Subject to revision.
-

- **Models:**
 - Conflicting.
 - Simplistic.
 - Incomplete.
- **Data:**
 - Random.
 - Biased, unknown correlations.
 - Subject to revision.
- **Time:**
 - Past may not reflect future.
 - Laws may change.

§ The art of designing, deciding, planning:

Use the **wrong model** and **data**

to make the **right decision**

(when the right model is unknown).

§ Info-gap decision strategies:

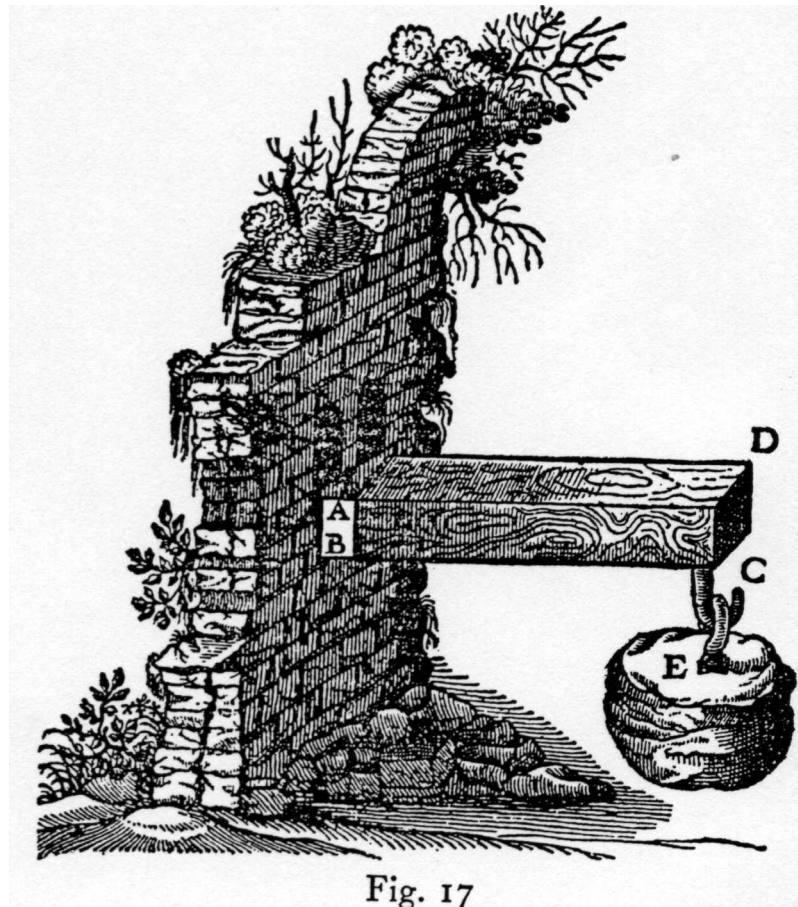
- **Robust-satisficing:** **protect against uncertainty.**
-

§ Info-gap decision strategies:

- **Robust-satisficing:** **protect against uncertainty.**
- **Opportune-windfalling:** **exploit uncertainty.**

2 *DESIGN of a VIBRATING CANTILEVER*

2.1 *Design Problem*



§ Galileo's Cantilever.

§ The cantilever is a paradigm for:

- Tall building.
- Radio tower.
- Crane.
- Airplane wing.
- Turbine blade.
- Diving board.
- Canon barrel.
- MEMS component.
- Atomic force microscope.
- etc.

§ **Goal: Restrain vibration** of cantilever
from **uncertain transient load**.

§

§ **Goal: Restrain vibration** of cantilever
from **uncertain transient load**.

§ **Two design concepts:**

- **Prevent** vibration by **stiffening** the beam.
- **Absorb** vibration by **dissipating** energy.

§

§ Goal: Restrain vibration of cantilever
from uncertain transient load.

§ Two design concepts:

- Prevent vibration by stiffening the beam.
- Absorb vibration by dissipating energy.

§ Not mutually exclusive.

§ Relevant to different circumstances.

2.2 *Robustness Function*

§ Three components of the analysis:

- **System** model.
- **Performance** criterion.
- **Uncertainty** model.

§ Simple system model:

Rigid vibration around clamped base.

$\theta(t)$ = angle of deflection of beam.

$u(t)$ = moment of force at base.

Equation of motion:

$$J \frac{d^2 \theta(t)}{dt^2} + c \frac{d\theta(t)}{dt} + k\theta = u(t)$$

$$J \frac{\mathrm{d}^2 \theta(t)}{\mathrm{d} t^2} + c \frac{\mathrm{d} \theta(t)}{\mathrm{d} t} + k \theta = u(t)$$

§ **Design variables:** $q = (c, k)$.

§ **System response:** $\theta(t, u, q)$.

§ Uncertainty model.

- What we **know** about the load:
 - The **nominal load**, $\tilde{u}(t)$.
 - The actual loads are **transient**:
 - May vary rapidly.
 - May deviate greatly from nominal load.
-

§ Uncertainty model.

- What we **know** about the load:
 - The **nominal** load, $\tilde{u}(t)$.
 - The actual loads are **transient**:
 - May vary rapidly.
 - May deviate greatly from nominal load.
- What we **don't know** about the load:
The **actual realization**, $u(t)$.

§ Info-gap model for uncertain transients:

$$\mathcal{U}(\textcolor{red}{h}, \widetilde{u}) = \left\{ \textcolor{red}{u}(t) : \int_0^\infty [\textcolor{red}{u}(t) - \widetilde{u}(t)]^2 \, dt \leq \textcolor{red}{h}^2 \right\}, \quad \textcolor{red}{h} \geq 0$$

$\textcolor{red}{h}$ = unknown horizon of uncertainty.

$\textcolor{red}{u}(t)$ = unknown actual load.

$\widetilde{u}(t)$ = known nominal load.

§ The **performance criterion**:

Deflection must not exceed critical value:

$$|\theta(t, u, q)| \leq \theta_c$$

§

§ The **performance criterion**:

Deflection must not exceed critical value:

$$|\theta(t, \textcolor{red}{u}, q)| \leq \theta_c$$

§ **Problem**:

- $u(t)$ **uncertain**.
- Unknown horizon of uncertainty h .

§ Problem:

- $u(t)$ **uncertain**.
- Unknown horizon of uncertainty h .

§ Robust-satisficing design strategy:

- Satisfy vibration requirement.
- Maximize robustness.
- Don't try to minimize deflection.

§

§ Problem:

- $u(t)$ **uncertain**.
- Unknown horizon of uncertainty h .

§ Robust-satisficing design strategy:

- Satisfy vibration requirement.
- Maximize robustness.
- Don't try to minimize deflection.

§ Robustness of design q :

- Max acceptable horizon of uncertainty.
- Max h at which $|\theta(t, u, q)| \leq \theta_c$ guaranteed.

§ Robustness of design q :

- Max acceptable horizon of uncertainty.
- Max h at which $|\theta(t, u, q)| \leq \theta_c$ guaranteed.

$$\widehat{h}(q, \theta_c) = \max \left\{ h : \left(\max_{u \in \mathcal{U}(h, \tilde{u})} \theta(t, u, q) \right) \leq \theta_c \right\}$$

§ Derivation of robustness:

• Info-gap model:

$$\mathcal{U}(\textcolor{red}{h}, \textcolor{blue}{\tilde{u}}) = \left\{ \textcolor{red}{u}(t) : \int_0^\infty [\textcolor{red}{u}(t) - \textcolor{blue}{\tilde{u}}(t)]^2 \, dt \leq \textcolor{red}{h}^2 \right\}, \quad \textcolor{red}{h} \geq 0$$

•

§ Derivation of robustness:

• Info-gap model:

$$\mathcal{U}(\textcolor{red}{h}, \textcolor{blue}{\tilde{u}}) = \left\{ \textcolor{red}{u}(t) : \int_0^\infty [\textcolor{red}{u}(t) - \textcolor{blue}{\tilde{u}}(t)]^2 dt \leq \textcolor{red}{h}^2 \right\}, \quad \textcolor{red}{h} \geq 0$$

• System ($\theta(0) = \dot{\theta}(0) = 0$) and performance requirement:

$$\begin{aligned} \theta_u(t) &= \int_0^t f(\tau) u(\tau) d\tau, \quad |\theta_u(t)| \leq \theta_c \\ &= \underbrace{\int_0^t f(\tau) [u(\tau) - \tilde{u}(\tau)] d\tau}_A + \int_0^t f(\tau) \tilde{u}(\tau) d\tau \end{aligned}$$

•

§ Derivation of robustness:

- **Info-gap model:**

$$\mathcal{U}(\textcolor{red}{h}, \textcolor{blue}{\tilde{u}}) = \left\{ \textcolor{red}{u}(\textcolor{red}{t}) : \int_0^\infty [\textcolor{red}{u}(\textcolor{red}{t}) - \textcolor{blue}{\tilde{u}}(\textcolor{blue}{t})]^2 \, dt \leq \textcolor{red}{h}^2 \right\}, \quad \textcolor{red}{h} \geq 0$$

- **System ($\theta(0) = \dot{\theta}(0) = 0$) and performance requirement:**

$$\begin{aligned} \theta_u(t) &= \int_0^t f(\tau) u(\tau) \, d\tau, \quad |\theta_u(t)| \leq \theta_c \\ &= \underbrace{\int_0^t f(\tau) [u(\tau) - \tilde{u}(\tau)] \, d\tau}_A + \int_0^t f(\tau) \tilde{u}(\tau) \, d\tau \end{aligned}$$

- **Cauchy-Schwarz inequality:**

$$\left(\int a(t) b(t) \, dt \right)^2 \leq \int a^2(t) \, dt \int b^2(t) \, dt, \quad \text{‘=’ if } a(t) \propto b(t)$$

-

§ Derivation of robustness:

- **Info-gap model:**

$$\mathcal{U}(\textcolor{red}{h}, \textcolor{blue}{\tilde{u}}) = \left\{ \textcolor{red}{u}(t) : \int_0^\infty [\textcolor{red}{u}(t) - \textcolor{blue}{\tilde{u}}(t)]^2 dt \leq \textcolor{red}{h}^2 \right\}, \quad \textcolor{red}{h} \geq 0$$

- **System ($\theta(0) = \dot{\theta}(0) = 0$) and performance requirement:**

$$\begin{aligned} \theta_u(t) &= \int_0^t f(\tau) u(\tau) d\tau, \quad |\theta_u(t)| \leq \theta_c \\ &= \underbrace{\int_0^t f(\tau) [u(\tau) - \tilde{u}(\tau)] d\tau}_A + \int_0^t f(\tau) \tilde{u}(\tau) d\tau \end{aligned}$$

- **Cauchy-Schwarz inequality:**

$$\left(\int a(t) b(t) dt \right)^2 \leq \int a^2(t) dt \int b^2(t) dt, \quad \text{‘=’ if } a(t) \propto b(t)$$

- **Use Cauchy-Schwarz inequality:**

$$A \leq \sqrt{\int f^2(t) dt} \underbrace{\sqrt{\int [u(t) - \tilde{u}(t)]^2 dt}}_h$$

-

§ Derivation of robustness:

- **Info-gap model:**

$$\mathcal{U}(\textcolor{red}{h}, \textcolor{blue}{\tilde{u}}) = \left\{ \textcolor{red}{u}(t) : \int_0^\infty [\textcolor{red}{u}(t) - \textcolor{blue}{\tilde{u}}(t)]^2 dt \leq \textcolor{red}{h}^2 \right\}, \quad \textcolor{red}{h} \geq 0$$

- **System ($\theta(0) = \dot{\theta}(0) = 0$) and performance requirement:**

$$\begin{aligned} \theta_u(t) &= \int_0^t f(\tau) u(\tau) d\tau, \quad |\theta_u(t)| \leq \theta_c \\ &= \underbrace{\int_0^t f(\tau) [u(\tau) - \tilde{u}(\tau)] d\tau}_A + \int_0^t f(\tau) \tilde{u}(\tau) d\tau \end{aligned}$$

- **Cauchy-Schwarz inequality:**

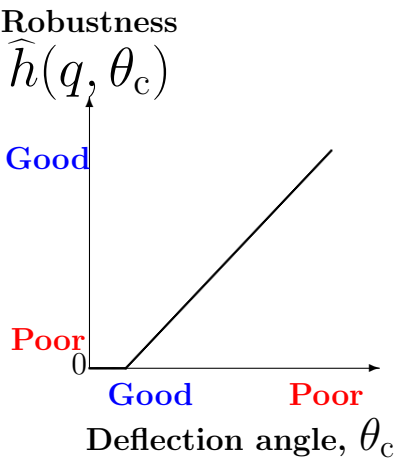
$$\left(\int a(t) b(t) dt \right)^2 \leq \int a^2(t) dt \int b^2(t) dt, \quad \text{‘=’ if } a(t) \propto b(t)$$

- **Use Cauchy-Schwarz inequality:**

$$A \leq \sqrt{\int f^2(t) dt} \underbrace{\sqrt{\int [u(t) - \tilde{u}(t)]^2 dt}}_h$$

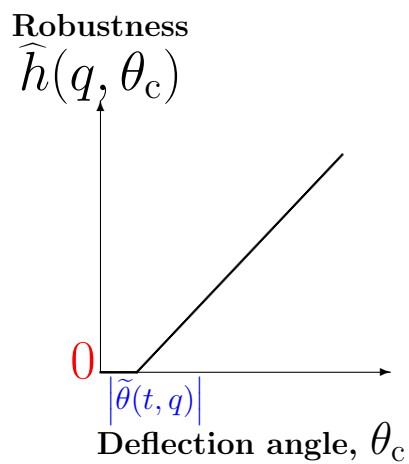
- **Thus:**

$$\widehat{h}(q, \theta_c) = \frac{\theta_c - |\tilde{\theta}(t, q)|}{\sqrt{\int_0^t f^2(\tau, q) d\tau}} \quad \text{if } \theta_c \geq |\tilde{\theta}(t, q)|$$



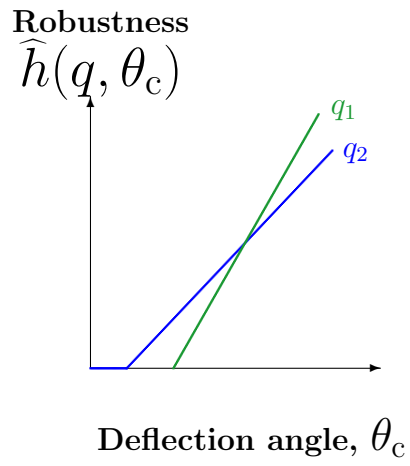
§ Trade-off: robustness vs. performance.

$$\widehat{h}(q,\theta_c)=\left\{\begin{array}{ll}\frac{\theta_c-|\widetilde{\theta}(t,q)|}{\sqrt{\int_0^t f^2(\tau,q)\,\mathrm{d}\tau}} & \text{if } \theta_c\geq |\widetilde{\theta}(t,q)| \\ 0 & \text{else}\end{array}\right.$$

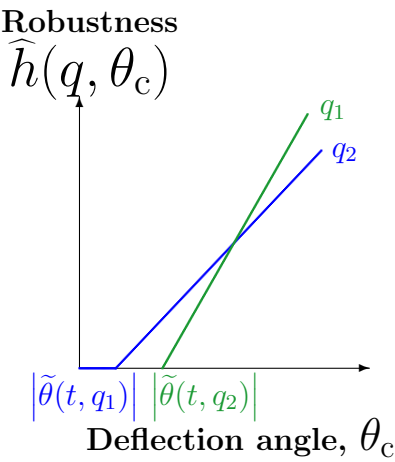


§ **Zeroing:** Estimated performance has no robustness:

$$\hat{h}(q, \theta_c) = 0 \quad \text{if} \quad \theta_c = |\tilde{\theta}(t, q)|$$



§ Two designs: q_1 and q_2 .

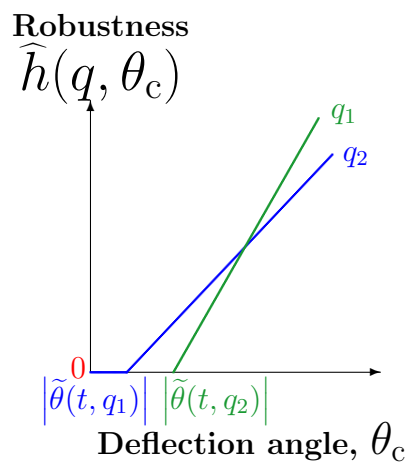


§ Best-model preference:

$$|\tilde{\theta}(t, q_1)| < |\tilde{\theta}(t, q_2)|$$

implies:

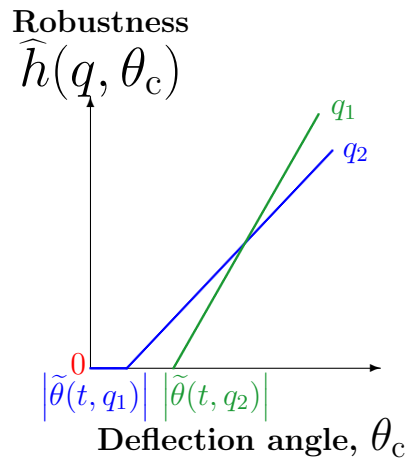
$$q_1 \succ q_2$$



§ Best-model preference has **no robustness**:

$$\widehat{h}(q_1, \theta_c) = 0 \quad \text{if} \quad \theta_c = | \widetilde{\theta}(t, q_1) |$$

Thus ...



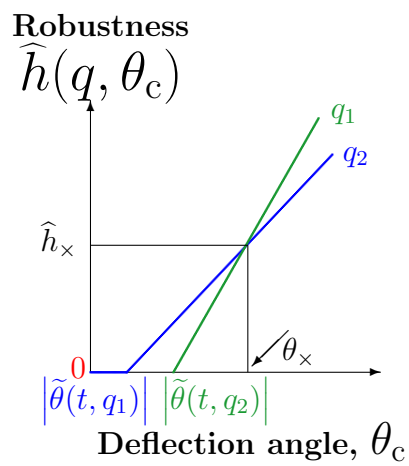
§ **Best-model preference has no robustness:**

$$\widehat{h}(q_1, \theta_c) = 0 \quad \text{if} \quad \theta_c = |\widetilde{\theta}(t, q_1)|$$

Thus

$$|\widetilde{\theta}(t, q_1)| < |\widetilde{\theta}(t, q_2)|$$

is not a good basis for preferring q_1 .



§ Best-model preference: $q_1 \succ q_2$.

§ Preference reversal: $q_2 \succ q_1$
if θ_x is adequate.

2.3 *Numerical Example*

§ **Nominal input:** Time-varying load.

- Estimated input, $\tilde{u}(t)$, is square:

$$\tilde{u}(t) = \begin{cases} \tilde{u}_o, & 0 \leq t \leq T \\ 0, & t > T \end{cases}$$

-

§ **Nominal input:** Time-varying load.

- Estimated input, $\tilde{u}(t)$, is square:

$$\tilde{u}(t) = \begin{cases} \tilde{u}_o, & 0 \leq t \leq T \\ 0, & t > T \end{cases}$$

- True input, $u(t)$, is uncertain.

§

§ Nominal input: Time-varying load.

- Estimated input, $\tilde{u}(t)$, is square:

$$\tilde{u}(t) = \begin{cases} \tilde{u}_o, & 0 \leq t \leq T \\ 0, & t > T \end{cases}$$

- True input, $u(t)$, is uncertain.

§ Robust-satisficing design strategy:

- Satisfy vibration requirement.
- Maximize robustness.
- Don't try to optimize (minimize) deflection.

§ Design variables:

- $q = (c, k)$: damping and stiffness.
- ζ = dimensionless damping.
- ω = natural frequency.

§

§ Design variables:

- $q = (c, k)$: damping and stiffness.
- ζ = dimensionless damping.
- ω = natural frequency.

§ Consider 6 designs:

- $\omega = 1, 3, 4.$ $\zeta = 0.01.$
- $\zeta = 0.03, 0.3, 0.5.$ $\omega = 1.$

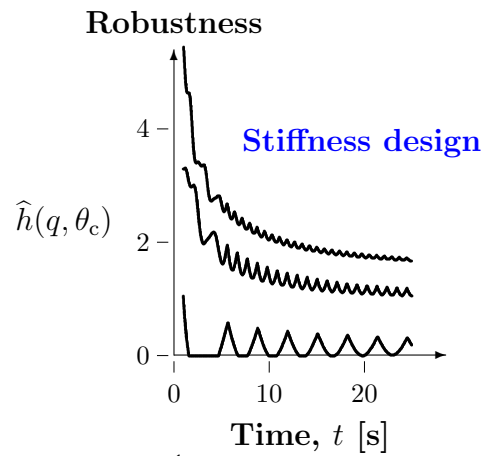


Figure 1: $\omega = 1, 3$ and 4 (bottom to top). $\zeta = 0.01$.

§ Variable stiffness; low damping:

- \hat{h} oscillates and decreases over time.
- Low stiffness ($\omega = 1$): \hat{h} periodically zero.
- Moderate and high stiffness ($\omega = 3, 4$):
 \hat{h} oscillates but positive.
- Large \hat{h} at $t < T$.

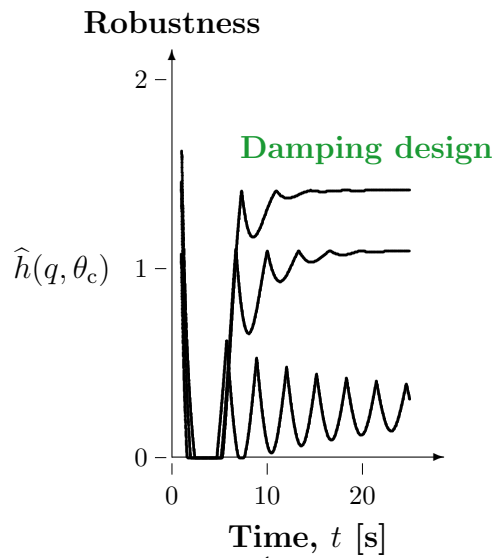
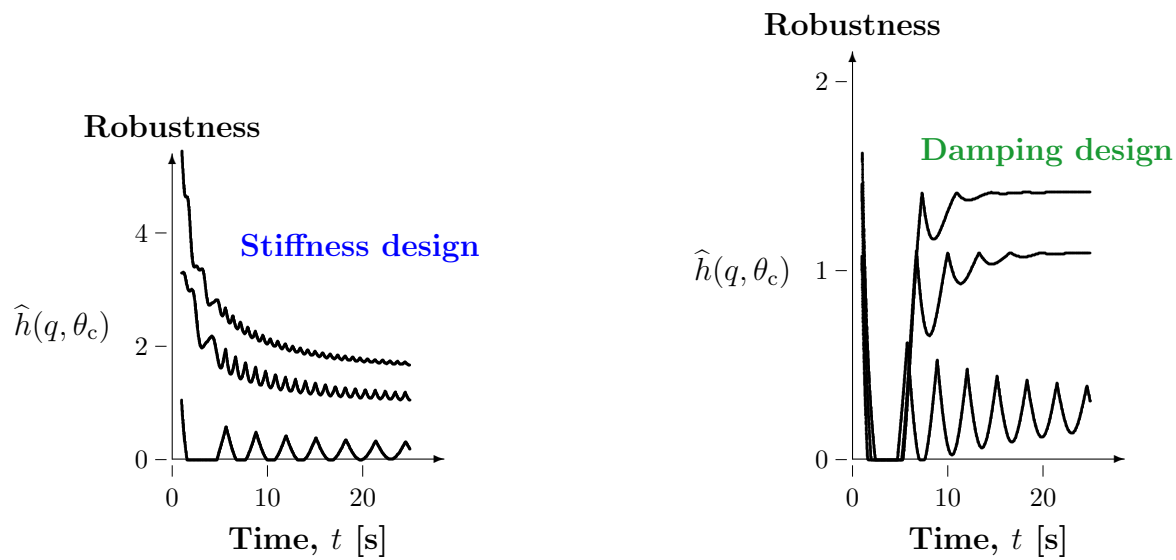


Figure 2: $\zeta = 0.03, 0.3, 0.5$ (bottom to top). $\omega = 1$.

§ Variable damping; low stiffness:

- Low damping: same as before.
- Large damping ($\zeta = 0.3$ or 0.5):
 - \hat{h} small for $t \leq T$.
 - \hat{h} large and constant for $t > T$.



§ Design implications:

Time frame determines design concept:

- $t < T$: **stiffness** design.
- $t > T$: **dissipation** design.
- $t > 0$: combined **stiff.** & **dissip.** design.

2.4 *Opportuneness Function*

§ **Windfall reward:** angular deflection θ_{w}
much less than critical requirement, θ_{c} :

$$\theta_{\text{w}} \ll \theta_{\text{c}}$$

§ Opportuneness of design q :

- Minimum promising horizon of uncertainty.
- Minimum h at which $|\theta(t, u, q)| \leq \theta_w$ possible.

$$\widehat{\beta}(q, \theta_w) = \min \left\{ h : \left(\min_{u \in \mathcal{U}(h, \tilde{u})} \theta(t, u, q) \right) \leq \theta_w \right\}$$

§ Compare **opportuneness** and **robustness**.

§ **Opportuneness** of design q :

- **Minimum promising** horizon of uncertainty.
- **Minimum** h at which **windfall possible**.

$$\widehat{\beta}(q, \theta_w) = \min \left\{ h : \left(\min_{u \in \mathcal{U}(h, \tilde{u})} \theta(t, u, q) \right) \leq \theta_w \right\}$$

§ **Robustness** of design q :

- **Maximum acceptable** horizon of uncertainty.
- **Maximum** h at which **critical requirement guaranteed**.

$$\widehat{h}(q, \theta_c) = \max \left\{ h : \left(\max_{u \in \mathcal{U}(h, \tilde{u})} \theta(t, u, q) \right) \leq \theta_c \right\}$$

§ Opportuneness function:

$$\widehat{\beta}(q, \theta_{\text{w}}) = \begin{cases} \frac{|\widetilde{\theta}(t, q)| - \theta_{\text{w}}}{\sqrt{\int_0^t f^2(\tau, q) \, \mathrm{d}\tau}} & \text{if } \theta_{\text{w}} \leq |\widetilde{\theta}(t, q)| \\ 0 & \text{else} \end{cases}$$

§ Compare opportuneness to robustness:

$$\widehat{\beta}(q, \theta_{\text{w}}) = -\widehat{h}(q, \theta_{\text{c}}) + \frac{\theta_{\text{c}} - \theta_{\text{w}}}{\sqrt{\int_0^t f^2(\tau) \, \mathrm{d}\tau}}$$

§ Antagonism or sympathy of immunity functions?

- $\widehat{h}(q, \theta_{\text{c}})$: Bigger is better.
- $\widehat{\beta}(q, \theta_{\text{w}})$: Big is bad.
-

§ Compare opportuneness to robustness:

$$\widehat{\beta}(q, \theta_w) = -\widehat{h}(q, \theta_c) + \frac{\theta_c - \theta_w}{\sqrt{\int_0^t f^2(\tau) d\tau}}$$

§ Antagonism or sympathy of immunity functions?

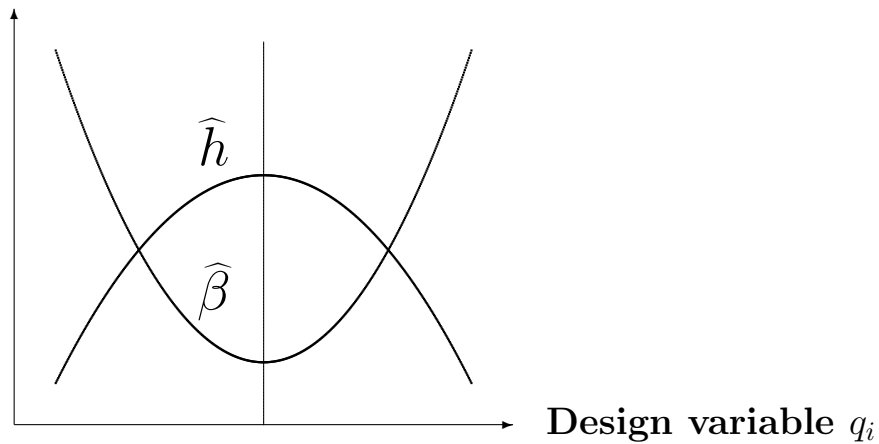
- $\widehat{h}(q, \theta_c)$: Bigger is better.
- $\widehat{\beta}(q, \theta_w)$: Big is bad.
- $q = (\omega, \zeta)$ design vector.
- $\widehat{\beta}(q, \theta_w)$ and $\widehat{h}(q, \theta_c)$ are sympathetic if they can be improved simultaneously.
- Antagonistic otherwise.

§ \widehat{h} and $\widehat{\beta}$ **always sympathetic**

if and only if their **optima coincide**.

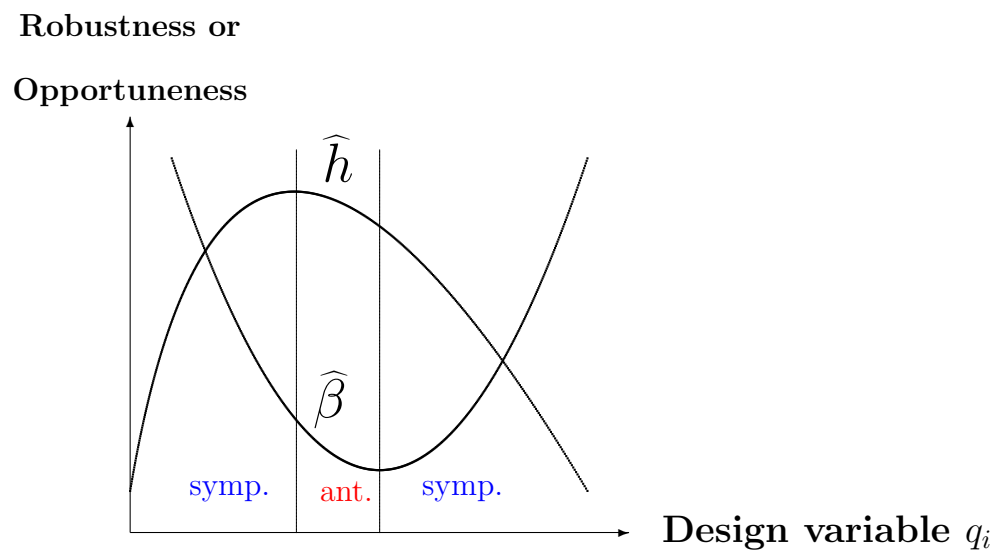
Robustness or

Opportuneness



§ “Usually” this will not happen.

§ Usually:



2.5 *Summary of Vibrating Cantilever Example*

§ Use load-estimate to choose design.

§

§ Use load-estimate to choose design.

§ Load-estimates err: info-gaps.

Hence: require robustness.

§

§ Use load-estimate to choose design.

§ Load-estimates err: info-gaps.

Hence: require robustness.

§ Load-estimate design: zero robustness.

§

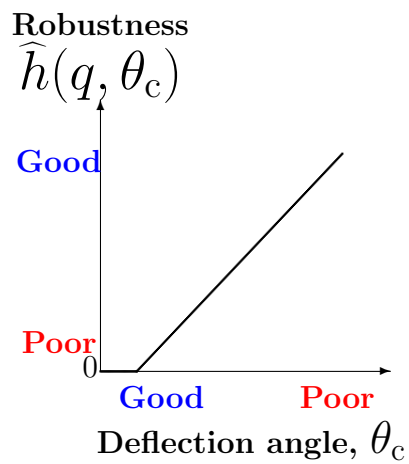
§ Use load-estimate to choose design.

§ **Load-estimates err:** info-gaps.

Hence: **require robustness.**

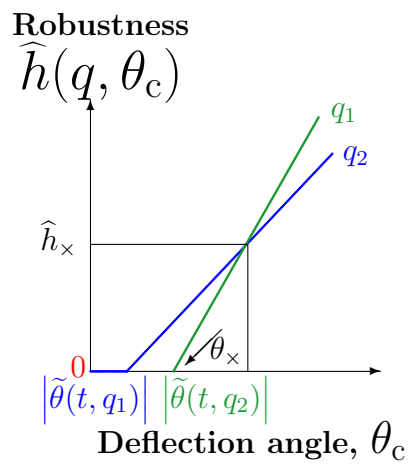
§ Load-estimate design: **zero robustness.**

§ Robustness **trades-off against** performance.



§ Robustness curves may cross:

Preference reversal.



§ Robust-satisficing design strategy:

- Satisfice vibration requirement.
- Maximize robustness to failure.

§

§ Robust-satisficing design strategy:

- Satisfice vibration requirement.
- Maximize robustness to failure.

§ Opportune-windfalling design strategy:

- Seek wonderful vibration outcome.
- Minimize immunity to windfall.

§

§ Robust-satisficing design strategy:

- Satisfice vibration requirement.
- Maximize robustness to failure.

§ Opportune-windfalling design strategy:

- Seek wonderful vibration outcome.
- Minimize immunity to windfall.

§ Robustness and opportuneness may be sympathetic or antagonistic.

3 SUMMARY

§ Models:

Attributes of model correspond to attributes of reality.

§ Model-based decision:

Adapt decision to attributes of model.

§ Optimization:

Use best model to choose decision with best outcome.

§

§ Models:

Attributes of model correspond to attributes of reality.

§ Model-based decision:

Adapt decision to attributes of model.

§ Optimization:

Use best model to choose decision with best outcome.

§ But there is **deep uncertainty**:

- **Randomness**: structured uncertainty.
- **Info-gaps**: surprises, ignorance.

§ **Fallacy** of optimal model-based decision:

- Severe uncertainty:
 - Best model errs seriously.
 - Some model attributes are **correct**.
 - Some model attributes **err greatly**.
- Best-model optimization
 - exploits **all model attributes** to extreme.
 - Vulnerable to model error.

§ Resolution: Info-gap decision theory.

- Satisfice performance.
- Optimize robustness to uncertainty.
- Model and manage sur^Prises.

§

§ Resolution: Info-gap decision theory.

- Satisfice performance.
- Optimize robustness to uncertainty.
- Model and manage sur^Prises.

§ Robust-satisficing syllogism:

- Adequate performance is necessary.
- More reliable adequate performance is better than less reliable adeq. perf.
- Thus maximum reliability is best.

§

§ Resolution: Info-gap decision theory.

- Satisfice performance.
- Optimize robustness to uncertainty.
- Model and manage sur^Prises.

§ Robust-satisficing syllogism:

- Adequate performance is necessary.
- More reliable adequate performance is better than less reliable adeq. perf.
- Thus maximum reliability is best.

§ Opportune windfalling:

Exploit uncertain opportunities.

§ Sources: <http://info-gap.technion.ac.il>

§ Applications of info-gap theory:

- Monetary economics.
- Financial stability.
- Public policy and regulation.
- Climate change.
- Engineering design.
- Biological conservation.
- Sampling, assay design.
- Medical decision making.
- Fault detection and diagnosis.
- Project management.
- Homeland security.
- Statistical hypothesis testing.